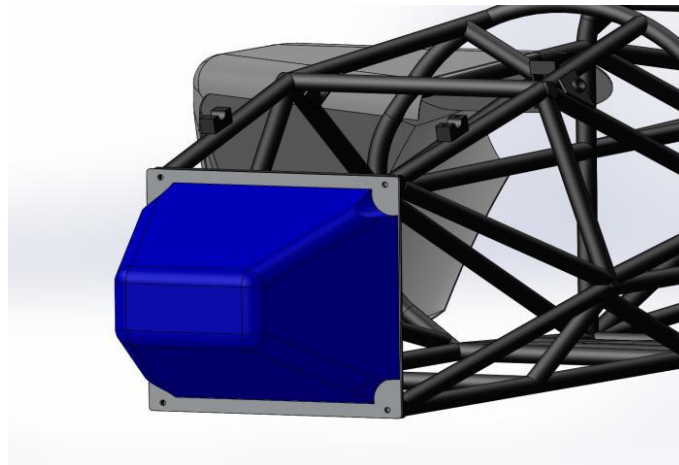


# 2024 SES (Structural Equivalency Spreadsheet) guidance

## F.8 Front Protection



There are 4 choices for IA, and the test method should follow each type.

BLANK

Attenuator and Diagonal

No Test: +

F.8.4.1	Impact Attenuator Type:	BLANK	4折	BLANK
	Standard Foam Attenuator Height:	304mm (12in)	N/A	
	Standard Foam Attenuator Width:	355mm (14in)	N/A	
F.8.4.3	Front Bulkhead Outside to Outside Height:	mm	BLANK	
	Front Bulkhead Outside To Outside Width:	mm	BLANK	

BLANK

F.8.4.3	Diagonal Tube, Attenuator Test, or Composite	BLANK	EQ
	Minimum Tube Used		
F.3.2.1	Example: 25.4mm x 1.2mm round	Steel	BLANK
F.3.4.1	Diagonal Minimum Tube:	Size C	BLANK
	Wall thickness:	1.2 mm	BLANK
F.3.4.1	Square side:	25 mm	BLANK
	Wall thickness:	0.0012 m	EQ
	Square side:	0.025 m	EQ
	Tube cross sectional area (A):	9.10E-05 m^2	EQ
	Tube second moment of inertia (I):	6.70E-09 m^4	EQ
F.3.4.2	Young's Modulus (E):	2.00E+11 0.00E+00 Pa	BLANK
F.3.5	Critical Buckling Modulus	Sy: 3.05E+08 0.00E+00 Pa	BLANK
	Sy:	E_1*I_1/L_1 <= E_2*I_2/L_2: 1.34E+03	EQ
	Bending Deflection	S_1*A_1/L_1 <= S_2*A_2/L_2: 2.78E+04	EQ
	Energy	4*S_1*I_1/L_1 <= 4*S_2*I_2/L_2/r: 6.43E+02	EQ
		Bending_1/(48*EI): 1.00E-02	EQ
		45*Bending^2/(48*EI): 3.22E+00	EQ

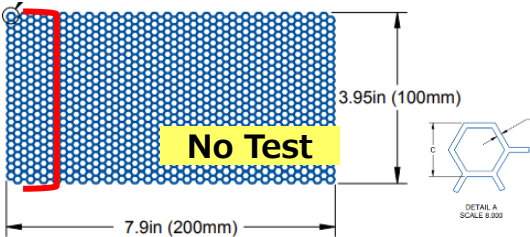
- Standard Foam
- Standard Honeycomb
- Custom-Non-Composite
- Custom-Composite : Meaning of monocoque structure

There are 4 types of test methods depending on the IA type.

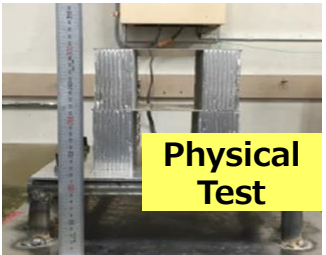
- No Test: Standard Foam + Matched FB
- No Test: Standard Honeycomb +
- Physical Test: Custom IA + AIP + FB Replica
- Dynamic Test: Composite IA + AIP + FB Replica



No Test



No Test



Physical Test



Dynamic Test

Select answers for all questions

Attach the requested evidence

Insert Pictures - may be added left or below:

(a.) Standard Impact Attenuator Receipt

(b.) Adhesive Material Properties -

Indicate selected value, include units conversion

(c.) Composite Material Receipts

(if not already on 3-Point test tab)

These are examples and the format does not matter.

**Invoice**

**BSCI Inc.**  
170 Balfour Park Lane  
Mooreville, NC 28115 USA  
Phone: (704) 664-3005  
Fax: (704) 660-1540

**PAID 12-19-2017**

**Ship To:**  
TOKYO UNIVERSITY OF SCIENCE YAMAGUCHI  
TAKAO KIJIMA  
1-1 TAMAOKUCHI SAN'YOUNGDA-SHI YAMAGUCHI  
SAN'YOUNGDA 754-884 JAPAN

WO #	PO #	Terms	Rep	Ship Date	Ship Via	Tracking #
8891		CRA		12/20/2017	UPS World Exp.	SEE BELOW

Item	Description	Backordered	Qty	Rate	Amount
FXM Attenuator	STANDARD IMPACT ATTENUATOR, MATERIAL DOW IMPACT 700		15	\$80.00	2,400.00
SHIPPING	SHIPPING CHARGES - UPS				
	INSURANCE EXPENSE				
	AVAILABLE, WITH 1,500 5-7				
	IN WORKING DAYS FOR				
	DELIVERY				

**Subtotal** \$4,270.00  
**Sales Tax (0.0%)** \$0.00  
**Payments/Credits** -\$4,270.00  
**Balance** \$0.00

**TECHNICAL SHEET CEMEDINE**

**二液常温硬化型エポキシ系接着剤**  
**セメダイン EP-007 (クリアタイプ)**  
**セメダイン EP-008 (クリア/止めタイプ)**

SG-EPOシリーズは、全く新しいタイプの二液常温硬化型エポキシ系接着剤です。SG (Second Generation=第二世代) エポキシの名前のとおり、従来のエポキシ系接着剤の欠点(たとえば、はく離層、耐熱性)を改良し、構造用接着剤に匹敵する性能を有しています。

**特長**

- ① はく離層が大きい。
- ② 耐熱性が良い。
- ③ 耐熱性が良好である。
- ④ オープンタイプをとっても、強度が低下しない。
- ⑤ 接着性が良好である。

**用途**

樹脂、プラスチック、ガラスなどの硬質材料の接着に使用します。

**性状 EP-007**

項目	単位	値
粘度 (25℃)	Pa·s	0.01
弾性率 (25℃)	GPa	2.5
引張強度 (25℃)	MPa	15
引張伸び (25℃)	%	10
引張率 (25℃)	MPa	150
引張率 (25℃)	MPa	150

**性状 EP-008**

項目	単位	値
粘度 (25℃)	Pa·s	0.01
弾性率 (25℃)	GPa	2.5
引張強度 (25℃)	MPa	15
引張伸び (25℃)	%	10
引張率 (25℃)	MPa	150
引張率 (25℃)	MPa	150

**プリブレグ検査表**  
CERTIFICATE OF CONFORMITY

**三菱ケミカル株式会社**  
MITSUBISHI CHEMICAL CORPORATION

検査日 2019.11.25  
INSPECTION DATE

品名 CSテープ  
品番 TR 350G100SB4ZFW5

SIZE W: 1000mm L: 125m (125m<sup>2</sup>)

LOT NO MA958B

CASE NO MA958B-03

項目 (ITEM)	測定値 (LOT AV.)
プリブレグ目付 (g/m <sup>2</sup> ) (PAW)	151.0
乾燥目付 (g/m <sup>2</sup> ) (PAW)	100.6
樹脂含有率 (wt%) (R/C)	33.4

**APPEARANCE INSPECTION**

欠陥名 (DEFECT TYPE)	欠陥個数 (NO OF DEFECT)	補償長 (m)
その他 (OTHER)	1	0.5

合計 (TOTAL) 1 0.5

検査員 (INSPECTOR)

合格

Attach the requested evidence

BLANK				
F.8.4.3	Diagonal Tube, Attenuator Test, or Composite	Minimum	Tube Used	BLANK
F.3.2.1	Example: 25.4mm x 1.2mm round	Steel		N/A
F.3.4.1	Diagonal Minimum Tube:	Size C		N/A
	Wall thickness:	1.2	mm	N/A
F.3.4.1	Square side:	25	mm	N/A

**F.8.4.3.a** Tube frame teams should weld a diagonal to the Front Bulkhead.  
**F.8.4.3.a** Monocoque teams should install diagonals with 2" x 30kN attachment to reduce twisting. The structure must go across the entire front bulkhead opening on the diagonal. If a front bulkhead or removable panel with no openings is not feasible, preferably a square tube is welded or bonded to the AIP. Round tubes may not be welded or bonded to the

Diagonal, AIP, and FB material must be entered in cells J57, J59, T37, AN35, and AN37.

If Diagonal is required for FBH in Standard IA, don't forget to input these as well.

Physical test is required for Composite AIP

No additional test for Steel or Aluminum AIP.

BLANK			
F.8.2.1	Anti-Intrusion Plate (AI) material:	Steel	EQ
	Steel: 1.5mm (0.060in), Aluminum: 4.0mm (0.157in):	mm	BLANK

- F.8.3.2 AI plates made of any material besides steel or aluminum must either:
- F.8.3.2.a Be physically tested on a replica bulkhead up to 120kN, with the load distributed over the 200 mm x 100mm minimum IA area.
- F.8.3.2.b Show F.8.3.4 120kN equivalence from F.4.3.1 laminate testing.

EQ			
F.8.3.2	Composite Anti Intrusion:	Steel	N/A
F.8.3.2	Composite AI Equivalence:		N/A
	Type SES Tab Name Of Layup Used:		N/A
F.4.3.2.d	50% < Core < 100%:	Type	Core thickness: mm
	Scaling option, layup repeats:	Outer skin thickness: Layup	mm
	Scaling option, layup repeats:	Inner skin thickness: Type	mm
		Thickness of panel: #VALUE!	mm
		Composite Panel Height:	mm
		Composite Panel Width:	mm
		Top Edge of FB to Top Edge of IA:	mm
F.8.3.1	Minimum Required Impact Attenuator Height:	100	mm
	Minimum Required Impact Attenuator Width:	200	mm
	Second moment of inertia I, Vertical:	m^4	N/A
	Second moment of inertia I, Horizontal:	m^4	N/A
	Young's Modulus (E):	Layup	Pa
	Ultimate Tensile Strength (S):	Name	Pa
	Shear:	Type	Pa
F.8.3.1	Max Bending Moment, Vertical (120kN Partial UDL):		Nm
	Max Bending Moment, Horizontal (120kN Partial UDL):		Nm
	Max Bending * Max y / I = Max Stress, Vertical:	Pa	N/A
	Max Bending * Max y / I = Max Stress, Horizontal:	Pa	N/A
	UTS (S) / Max Stress = Safety Factor, Bending:		N/A
	Perimeter Shear Stress, 120kN Load:	Pa	N/A
	Safety Factor, Perimeter Shear:		N/A

Composite AIP -

Physical test required

EQ			
F.8.2.1	Anti-Intrusion Plate (AI) material:	Composite	EQ
	Steel: 1.5mm (0.060in), Aluminum: 4.0mm (0.157in):	mm	N/A
F.8.3.2 - AIP 3-Point & Shear or 120kN Physical Test required.			

- F.8.3.2 AI plates made of any material besides steel or aluminum must either:
- F.8.3.2.a Be physically tested on a replica bulkhead up to 120kN, with the load distributed over the 200 mm x 100mm minimum IA area.
- F.8.3.2.b Show F.8.3.4 120kN equivalence from F.4.3.1 laminate testing.

BLANK			
F.8.3.2	Composite Anti Intrusion:	Composite	EQ
F.8.3.2	Composite AI Equivalence:		BLANK
	Type SES Tab Name Of Layup Used:		BLANK
F.4.3.2.d	50% < Core < 100%:	Type	Core thickness: mm
	Scaling option, layup repeats:	Outer skin thickness: Layup	mm
	Scaling option, layup repeats:	Inner skin thickness: Type	mm
		Thickness of panel: #VALUE!	mm
		Composite Panel Height:	mm
		Composite Panel Width:	mm
		Top Edge of FB to Top Edge of IA:	mm
	Minimum Required Impact Attenuator Height:	100	mm
	Minimum Required Impact Attenuator Width:	200	mm
	Second moment of inertia I, Vertical:	m^4	EQ
	Second moment of inertia I, Horizontal:	m^4	EQ
	Young's Modulus (E):	Layup	Pa
	Ultimate Tensile Strength (S):	Name	Pa
	Shear:	Type	Pa
	Max Bending Moment, Vertical (120kN Partial UDL):		Nm
	Max Bending Moment, Horizontal (120kN Partial UDL):		Nm
	Max Bending * Max y / I = Max Stress, Vertical:	Pa	EQ
	Max Bending * Max y / I = Max Stress, Horizontal:	Pa	EQ
	UTS (S) / Max Stress = Safety Factor, Bending:		EQ
	Perimeter Shear Stress, 120kN Load:	Pa	EQ
	Safety Factor, Perimeter Shear:		EQ

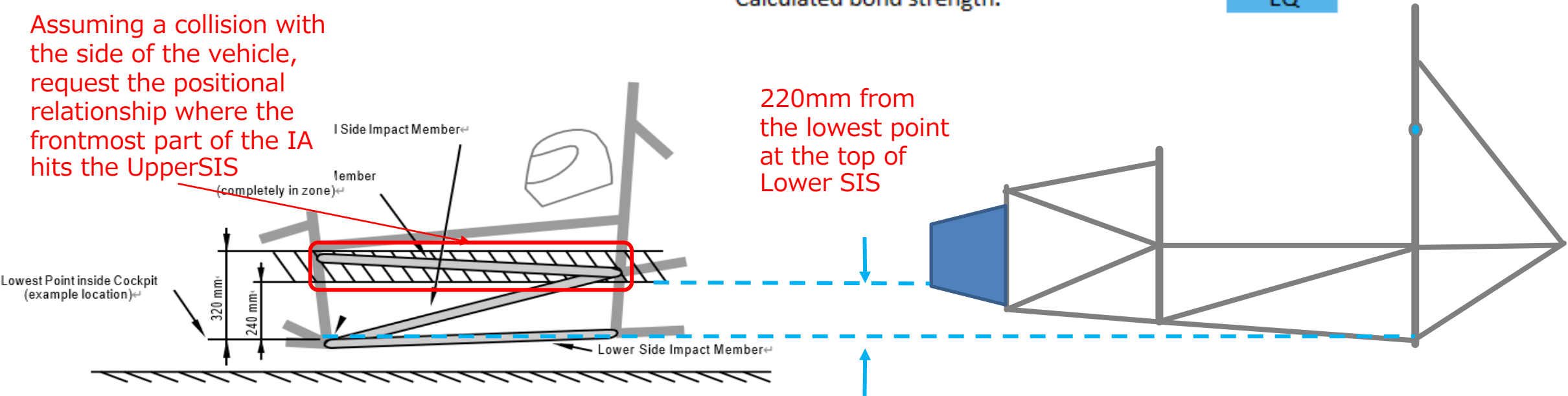
Added in 2024  
Added rules regarding  
core thickness

"BLANK" is not accepted  
Must be "EQ"



BLANK					
Ground clearance under lowest part of Lower SIS, setup ride height:		<input type="text"/>	mm	BLANK	
F.6.4.4.b	F.8.5.6.a	IA lower leading edge < 220mm above lower SIS:	<input type="text"/>	mm	BLANK
F.8.5.2		IA to AI plate mounting method:	Bonded		EQ
			<input type="text"/>		N/A
			<input type="text"/>	mm	N/A
What is the brand name of the adhesive?:			<input type="text"/>		BLANK
F.8.5.3.b		Minimum Bond Shear Requirement:	9.50E+04	N	EQ
		Minimum shear / peel strength of adhesive:	<input type="text"/>	N/mm^2	BLANK
F.5.5.3		50% adhesive reduction for safety factor:	0	N/mm^2	EQ
F.8.5.3.c		Minimum bond area:	<input type="text"/>	mm^2	BLANK
		Calculated bond strength:			EQ

Assuming a collision with the side of the vehicle, request the positional relationship where the frontmost part of the IA hits the UpperSIS



Attach the requested evidence Since each team has a different way of thinking and calculation methods, we will not provide specific examples.

Insert Pictures - continued:

(d.) Wing Detachment Material Properties

(e.) Other Wing Detachment Calculations  
(if not using standard fastener shear)

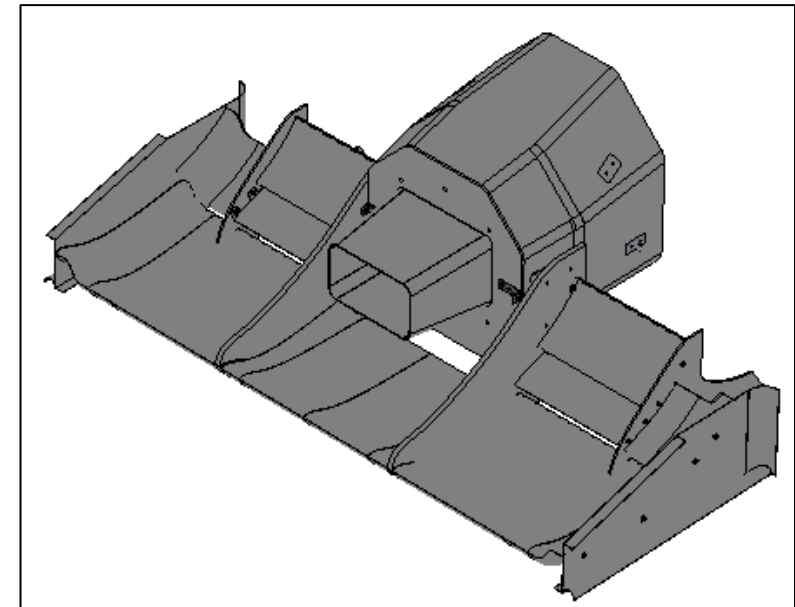
Insert measurement of IA front top edge height.

Shear Dimensions

Do not count holes as part of the area.  
Even with precrush, honeycomb bond area is  
usually <50% of the face.

**Regarding AIP and IA fixing methods, in addition to the isometric drawings below, enter detailed information on brackets, stays, bolts, etc. in a three-view drawing and attach it.**

**In previous years, many of these deficiencies are the cause of reexamination.**



The diagram cited is from Tokai University.  
It is an exemplary diagram, so I respectfully  
introduce it as a reference.

The concept when including the Front Wing is the same as before.

Please note that there are 5 types of Front Wing Mount Limit and the input items are different.

BLANK

Front Wing Mount Limit:  BLANK

No Front Wing N/A

Front Wing Physically Tested With IA N/A

Front Wing Physically Tested Without IA N/A

Fastener Shear Dialogue EQ

Wing Support Hand Calc EQ

F.8.8.2.a Peak deceleration force <= 120000N 95000 N EQ

Peak deceleration remains <= 40g: 32.3 g EQ

Front Wingが無い場合とIAと共に物理テストをした場合は項目選択以外の入力不要

EQ

Front Wing Mount Limit:  No Front Wing N/A

0 N N/A

0 N N/A

Peak Attenuator Force: 95000 N EQ

Peak deceleration force <= 120000N 95000 N EQ

Peak deceleration remains <= 40g: 32.3 g EQ

F.8.8.2.a

IA無しで物理テストをした場合、ファスナーの剪断力で計算する場合、その他独自の計算をする場合は、計算結果 + IAのピーク負荷で算出

BLANK

Front Wing Mount Limit:  Fastener Shear Dialogue EQ

Shear Diameter:  mm

Fastener UTS (Screenshot):  MPa BLANK

Total number of fasteners:  BLANK

Number\_of\_fasteners \* 0.577 \* UTS \* pi \* OD^2 / 4: 0 N BLANK

Peak Attenuator Force: 95000 N EQ

Peak deceleration force <= 120000N 95000 N EQ

Peak deceleration remains <= 40g: 32.3 g EQ

F.8.8.2.a

BLANK

Physical Tests

Insert Test Pictures - may be added below:

(a.) IA and FB test fixture before the test (F.8.7.4.d) which also shows the method of

If you did a physical test, please attach photos before and after the test and photos showing the experimental method.

(F.8.7.4.d) which shows the deflection was less than 25.4mm (F.8.7.6.d)

(c.) IA / AIP Force Displacement Curve

Paste in IA data from test below:

It is acceptable to resample the data at a lower frequency to reduce the number of datapoints.

MAX	MAX	AVERAGE	MAX
0	0	0	0
Disp.	Force	Weighted	Energy
mm	N	N	J
0	0	0	0
		#DIV/0!	0
		#DIV/0!	0
		#DIV/0!	0
		#DIV/0!	0
		#DIV/0!	0
		#DIV/0!	0

Paste in COMPOSITE AIP

data from test below:  
It is acceptable to resample the data at a lower frequency.

MAX	MAX

Paste in COMPOSITE AIP

data from test below:  
It is acceptable to resample the data at a lower frequency.

MAX	MAX

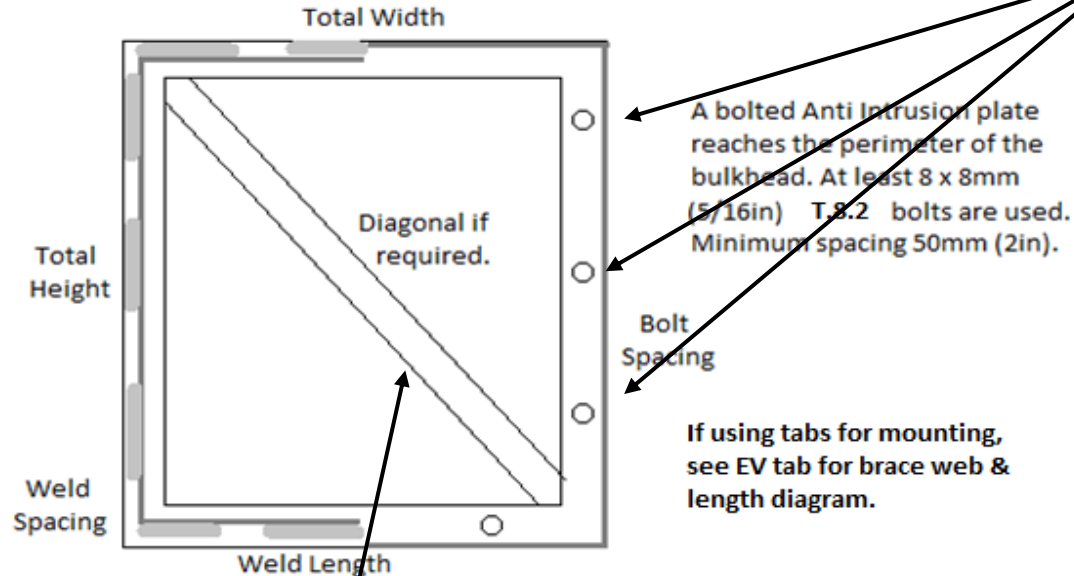
If you did a physical test, you will need to input the data of the experimental results.  
**\*Compressed data in 1mm increments is recommended.**



**REPLACE THIS EXAMPLE WITH YOUR OWN CAD.**

Include all required dimensions.

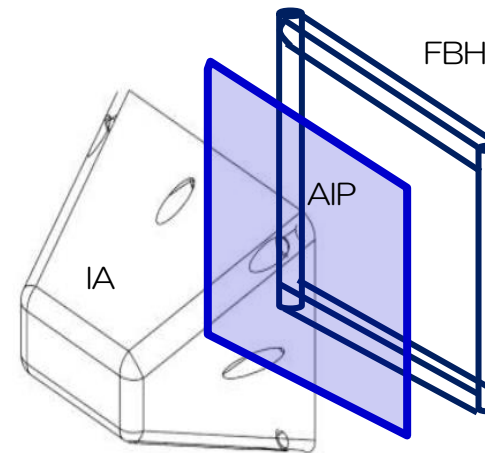
The Front Bulkhead shape may be more complex than this example.



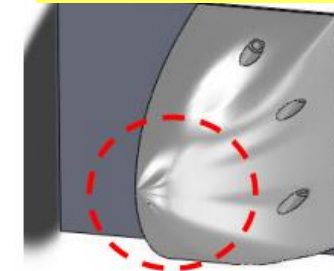
If not matched to the outside perimeter of the bulkhead, a welded Anti Intrusion plate reaches at least to the centerline of the bulkhead tubes. At least 50% of the plate perimeter is welded, with 25mm (1in) minimum welds.

When welding AIP, be able to calculate the ratio of welded and non-welded areas.

**When connecting bolts by directly drilling holes in BH → Put in the insert. (Regulation requirements)**

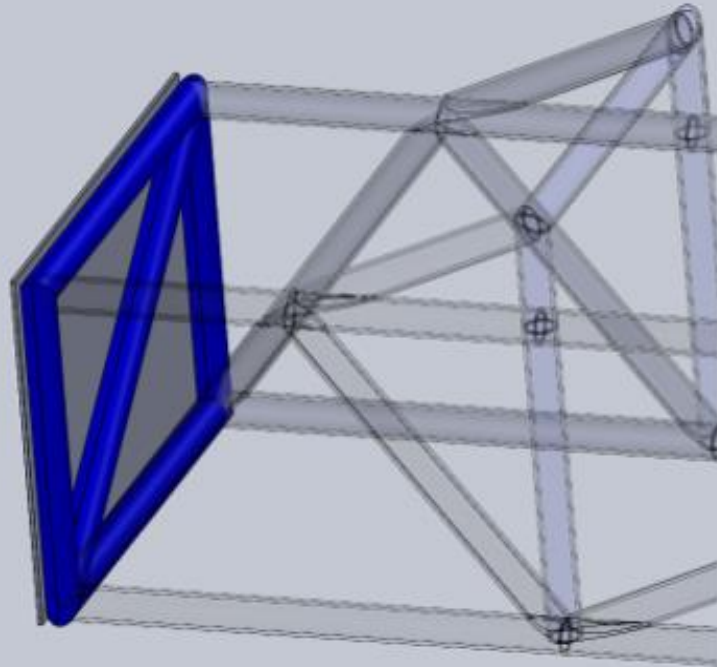


Standard IA prohibits any processing or shape modification

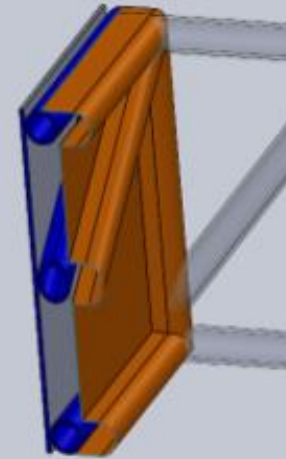
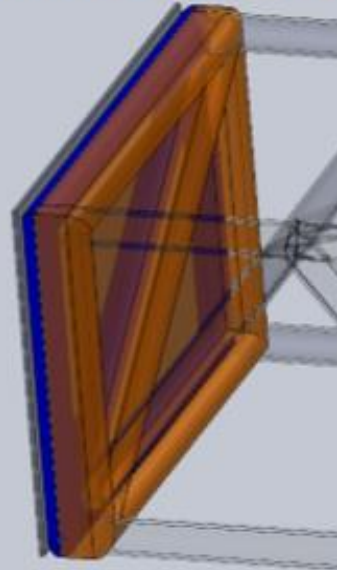


**NOT PERMITTED:** changed design or dimensions for Standard IA TYPE12

**F.8.4.3 Diagonal is required if standard IA (Form) with front bulkhead external dimensions greater than 400 x 350 mm and if standard IA (Honeycomb) is used.**



KEEP PEDALS AT FULL TRAVEL AT LEAST 25mm AWAY  
FROM REAR SURFACES OF FRONT BULKHEAD AND AIP



Front Bulkhead CAD with dimensions required.

Show 25mm gap to pedal assembly.

Pedal attachments preferably >25mm behind FB.

Attach a 3D CAD capture that proves that all pedals do not conflict with or enter the orange surface area shown above at full stroke (maximum adjustable range).

## Tube and composite have different input items

F.8.2.4 A 25mm gap is required between the AIP + FB + Diagonal and the pedal assembly.

BLANK			Tube	EQ
F.6.1	Front Bulkhead		Tube Used	EQ
F.3.2.1	Example: 25.4mm x 1.6mm round	Steel		BLANK
F.3.4.1	Front Bulkhead Minimum Tube:	Size B		BLANK
F.3.4.1	Wall thickness:	1.2	mm	BLANK
F.3.4.1	Square side:	25	mm	BLANK
F.3.4.1	Wall thickness:	0.0012	m	EQ
F.3.4.1	Square side:	0.025	m	EQ
F.3.4.1	Tube cross sectional area (A):	1.14E-04	m <sup>2</sup>	EQ
F.3.4.1	Tube second moment of inertia (I):	8.51E-09	m <sup>4</sup>	EQ
F.3.4.2	F.3.5	Young's Modulus (E):	2.00E+11	0.00E+00 Pa
F.3.5	Critical	S_Yield(S):	3.05E+08	0.00E+00 Pa
Buckling Modulus		E_1*I_1 <= E_2*I_2:	1.70E+03	EQ
S_Yield(S):		S_1*A_1 <= S_2*A_2:	3.48E+04	EQ
Bending		4*S_1*I_1/r <= 4*S_2*I_2/r:	8.17E+02	EQ
Deflection		Bending_1/(48*E):	1.00E-02	EQ
Energy		0.5*Bending^2/(48*E):	4.09E+00	EQ

In the case of "tube"

EQ			Tube	0	N/A
F.7.2	Front Bulkhead Construction:		Tube	0	N/A
F.7.2	Front Bulkhead Tubes Replaced Size B:	0	Diagonal Size C:	0	N/A
F.7.2	Type SES Tab Name Of Layout Used:				N/A
F.4.3.2.d	50% < Core < 100%:	Type	Core thickness:		N/A
F.4.3.2.d	Scaling option, layout repeats:		Outer skin thickness:	Layout	N/A
F.4.3.2.d	Scaling option, layout repeats:		Inner skin thickness:	Type	N/A
F.4.3.2.d			Thickness of panel:	#VALUE!	N/A
F.4.3.2.d			Front Bulkhead Height:		N/A
F.4.3.2.d			Front Bulkhead Width:		N/A
F.4.3.2.d			Cutout Height:		N/A
F.4.3.2.d			Cutout Width:		N/A
F.4.3.2.d			Composite Panel Height:	0	N/A
F.3.4.2.a		Young's Modulus (E):	2.00E+11	Layout	Pa
F.3.4.2.a		Ultimate Tensile Strength (S):	3.65E+08	Name	Pa
F.3.4.2.a		Shear:	2.11E+08	Type	Pa
F.7.2.2	25mm FBHS Section				N/A
F.7.2.2	Core thickness:	0	mm		N/A
F.7.2.2	Outer skin thickness:	0	mm		N/A
F.7.2.2	Inner skin thickness:	0	mm		N/A
F.7.2.2	Thickness of panel:	0	mm		N/A
F.3.4.2.a		Young's Modulus (E):	2.00E+11	0.00E+00	Pa
F.3.4.2.a		Ultimate Tensile Strength (S):	3.65E+08	0.00E+00	Pa
F.3.4.2.a		Shear:	2.11E+08	0.00E+00	Pa
F.3.2.1	Minimum FB wall thickness:	0.0012	0	m	N/A
F.3.4.1	Outer Diameter / Panel Thickness:	0.025	#VALUE!	m	N/A
F.3.4.1	Additive cross section (A):	0.00E+00	#VALUE!	m <sup>2</sup>	N/A
F.3.4.1	Additive second moment of inertia (I):	0.00E+00		m <sup>4</sup>	N/A
Buckling Modulus		E_1*I_1 <= E_2*I_2+E_3*I_3:	0.00E+00		N/A
UTS		S_1*A_1 <= S_2*A_2+S_3*A_3:	0.00E+00		N/A
Bending		4*S_1*I_1/r <= 4*(S_2*I_2+S_3*I_3)/r:	0.00E+00		N/A
Deflection		Bending_1/(48*E):	0.00E+00		N/A
Energy		F.4.3.2.3 comparison:	0.00E+00		N/A
F.7.3.3	1.5mm Steel Shear Equivalence:	3.16E+08			N/A

F.8.2.4 A 25mm gap is required between the AIP + FB + Diagonal and the pedal assembly.

EQ			Composite	EQ
F.6.1	Front Bulkhead		Composite	EQ
F.3.2.1	Example: 25.4mm x 1.6mm round	Steel		N/A
F.3.4.1	Front Bulkhead Minimum Tube:	Size B		N/A
F.3.4.1	Wall thickness:	1.2	mm	N/A
F.3.4.1	Square side:	25	mm	N/A
F.3.4.1	Wall thickness:	0.0012	m	N/A
F.3.4.1	Square side:	0.025	m	N/A
F.3.4.1	Tube cross sectional area (A):	1.14E-04	m <sup>2</sup>	N/A
F.3.4.1	Tube second moment of inertia (I):	8.51E-09	m <sup>4</sup>	N/A
F.3.4.2	F.3.5	Young's Modulus (E):	2.00E+11	0.00E+00 Pa
F.3.5	Critical	S_Yield(S):	3.05E+08	0.00E+00 Pa
Buckling Modulus		E_1*I_1 <= E_2*I_2:	1.70E+03	N/A
S_Yield(S):		S_1*A_1 <= S_2*A_2:	3.48E+04	N/A
Bending		4*S_1*I_1/r <= 4*S_2*I_2/r:	8.17E+02	N/A
Deflection		Bending_1/(48*E):	1.00E-02	N/A
Energy		0.5*Bending^2/(48*E):	4.09E+00	N/A

In case of "Composite"

BLANK			Composite	0	EQ
F.7.2	Front Bulkhead Construction:		Composite	0	EQ
F.7.2	Front Bulkhead Tubes Replaced Size B:	2	Diagonal Size C:	0	EQ
F.7.2	Type SES Tab Name Of Layout Used:				BLANK
F.4.3.2.d	50% < Core < 100%:	Type	Core thickness:		BLANK
F.4.3.2.d	Scaling option, layout repeats:		Outer skin thickness:	Layout	EQ
F.4.3.2.d	Scaling option, layout repeats:		Inner skin thickness:	Type	EQ
F.4.3.2.d			Thickness of panel:	#VALUE!	EQ
F.4.3.2.d			Front Bulkhead Height:		BLANK
F.4.3.2.d			Front Bulkhead Width:		BLANK
F.4.3.2.d			Cutout Height:		BLANK
F.4.3.2.d			Cutout Width:		BLANK
F.4.3.2.d			Composite Panel Height:	0	EQ
F.3.4.2.a		Young's Modulus (E):	2.00E+11	Layout	Pa
F.3.4.2.a		Ultimate Tensile Strength (S):	3.65E+08	Name	Pa
F.3.4.2.a		Shear:	2.11E+08	Type	Pa
F.7.2.2	25mm FBHS Section				EQ
F.7.2.2	Core thickness:	0	mm		EQ
F.7.2.2	Outer skin thickness:	0	mm		EQ
F.7.2.2	Inner skin thickness:	0	mm		EQ
F.7.2.2	Thickness of panel:	0	mm		EQ
F.3.4.2.a		Young's Modulus (E):	2.00E+11	0.00E+00	Pa
F.3.4.2.a		Ultimate Tensile Strength (S):	3.65E+08	0.00E+00	Pa
F.3.4.2.a		Shear:	2.11E+08	0.00E+00	Pa
F.3.2.1	Minimum FB wall thickness:	0.0012	0	m	EQ
F.3.4.1	Outer Diameter / Panel Thickness:	0.025	#VALUE!	m	EQ
F.3.4.1	Additive cross section (A):	2.28E-04	#VALUE!	m <sup>2</sup>	EQ
F.3.4.1	Additive second moment of inertia (I):	1.70E-08		m <sup>4</sup>	EQ
Buckling Modulus		E_1*I_1 <= E_2*I_2+E_3*I_3:	3.40E+03		EQ
UTS		S_1*A_1 <= S_2*A_2+S_3*A_3:	8.32E+04		EQ
Bending		4*S_1*I_1/r <= 4*(S_2*I_2+S_3*I_3)/r:	1.96E+03		EQ
Deflection		Bending_1/(48*E):	1.20E-02		EQ
Energy		F.4.3.2.3 comparison:	*****		*****
F.7.3.3	1.5mm Steel Shear Equivalence:	3.16E+08			EQ

Attach the requested evidence

There are 4 types of input options The contents of the filling are different depending on what you choose

## For Welded

BLANK		
F.8.2.2	AIP to FB Attachment: <input type="text" value="Welded"/>	EQ
AI plate must at least reach the centerline of Front Bulkhead tubes.		
F.8.2.3.a	At least half the perimeter must be welded: <input type="text" value=""/>	EQ
	Shortest weld >= 25mm (1in): <input type="text" value=""/>	BLANK
		BLANK

## For bolted

BLANK		
	AIP to FB Attachment: <input type="text" value="Bolted"/>	EQ
AI plate must match entire Front Bulkhead perimeter.		
F.8.2.3.b	Number of 8mm critical fasteners (8 required): <input type="text" value=""/>	EQ
	Minimum distance between bolt centers: <input type="text" value=""/>	BLANK
		BLANK

BLANK		
Bolting AIP to tube Front Bulkhead		
F.8.2.3.b	Locate AI bolts through FB tube inserts or on tabs: <input type="text" value="Nut And Bolt"/>	EQ
Maximum Fastener centerline offset from tube surface: <input type="text" value=""/>		
Mount cross section on tube surface: <input type="text" value="Quick Release"/>		
See diagrams: EV Acc tab AY28-B128		
	Mount thickness (B): <input type="text" value=""/>	BLANK
	Mount length (L): <input type="text" value=""/>	BLANK
	Mount thickness (T): <input type="text" value=""/>	BLANK
	Mount face (H): <input type="text" value=""/>	BLANK
	Mount <= Su-Weld: <input type="text" value=""/>	EQ
	Mount <= Su-Weld: <input type="text" value=""/>	EQ
	Mount <= Shear: <input type="text" value=""/>	EQ

If you select a bolt, two types of options will appear  
↑ Added in 2024

## For Bonded

BLANK		
Bonding AIP to composite Front Bulkhead		
F.8.2.3.c	Is there an opening in the Front Bulkhead? <input type="text" value=""/>	EQ
	What is the brand name of the adhesive? <input type="text" value=""/>	EQ
	Minimum shear / peel strength of adhesive: <input type="text" value=""/>	N/mm^2
F.5.5.3	50% adhesive reduction for safety factor: <input type="text" value="0"/>	N/mm^2
	Minimum bond area: <input type="text" value=""/>	mm^2
	Calculated bond strength: <input type="text" value=""/>	EQ

## For Laminated

BLANK		
Laminated AIP to composite Front Bulkhead		
F.8.2.3.d	Does the AIP form the front bulkhead of the monocoque? <input type="text" value=""/>	EQ
	Type SES Tab Name Of Enclosing Layup Used: <input type="text" value=""/>	BLANK
	Skin used: <input type="text" value=""/>	BLANK
	AIP Perimeter Length: <input type="text" value=""/>	mm
	Scaling option, layup repeats: <input type="text" value=""/>	Laminate thickness: <input type="text" value=""/>
		Typo mm
	Skin shear area - centerline x 1 thickness: <input type="text" value="#VALUE!"/>	m^2
	Skin shear strength: <input type="text" value="Typo"/>	Pa
F.8.2.3.d	Single tearout path >=120000N: <input type="text" value="0.00%"/>	EQ
	Front Hoop Lamination: <input type="text" value=""/>	BLANK
	Lap joint strength: <input type="text" value="Typo"/>	Pa
	Total bond width including both sides of the Front Hoop: <input type="text" value=""/>	mm
	Bond shear area: <input type="text" value="0"/>	m^2
F.8.2.3.d	Bond failure >=120000N: <input type="text" value="#VALUE!"/>	#VALUE!



If you select Quick Release, increase input items ⇒

BLANK		
Shear Calculation for Positive Locking on Quick Release		
	Positive Locking Shear Requirement	95000 N
Shear Diameter: <input type="text" value=""/>	Fastener UTS (Screenshot): <input type="text" value=""/>	MPa
	Number of positive locking diameters in shear: <input type="text" value=""/>	
	Number_of_fasteners * 0.577 * UTS * pi * OD^2 / 4:	0 0.00%

In the case of CentralLine Inserts, it is eligible for "Welded Inserts"

EQ

Bolting AIP to tube Front Bulkhead

Nut And Bolt

EQ

F.8.2.3.b

Locate AI bolts through FB tube inserts or on tabs:

Centerline Inserts

EQ

In the "F. 3. 4. 3 Welded Inserts" sheet, Aip Inserts is determined to "Yes", so enter into this sheet.

EQ

Any holes over 4mm drilled in

F.3.2.1 required tubes?

Tube Chassis BO124:

No

AIP Inserts:

Yes

EV Accumulator:

No

EQ

Does the steering rack

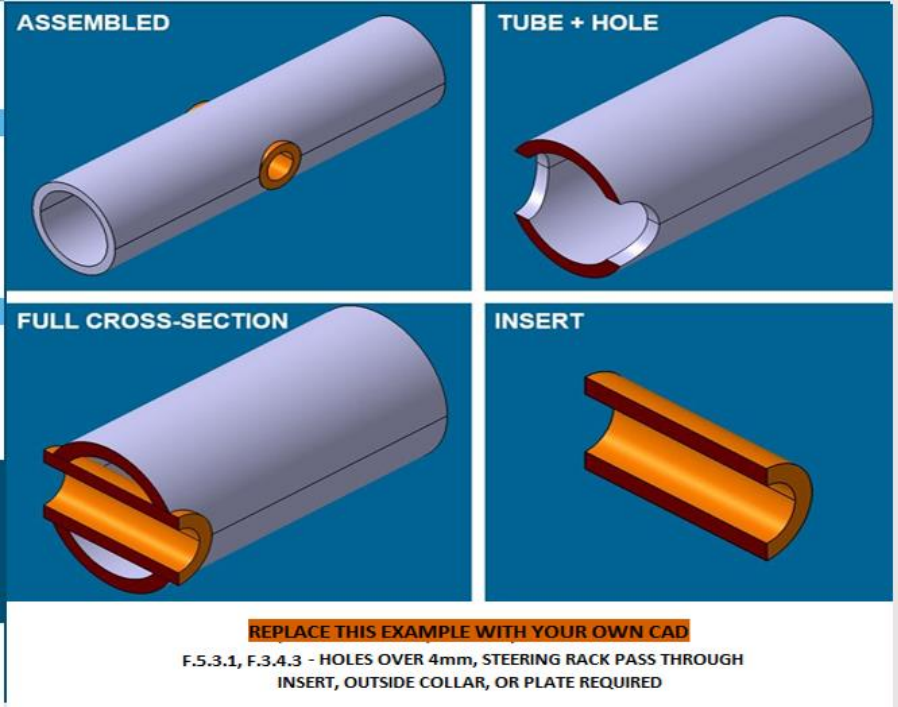
interrupt any required tubes?

Tube Chassis BO135:

No

FILL OUT THIS TAB.

BLANK





# 注意: AIP Attachment

## For "Offset Mounts"

F.8.2.3.b Locate AI bolts through FB tube inserts or on tabs:

Maximum Fastener centerline offset from tube surface:

Mount cross section on tube surface:

See diagrams: EV Acc tab AY28-BI28

Mount thickness (B):

Mount length (L):

Minimum gusset thickness (T):

Minimum gusset height normal to mount face (H):

F.3.5 0.0 15kN shear bending  $M*y / I \leq Su$ -Weld:

0.00E+00 0.0 15kN normal bending  $M*y / I \leq Su$ -Weld:

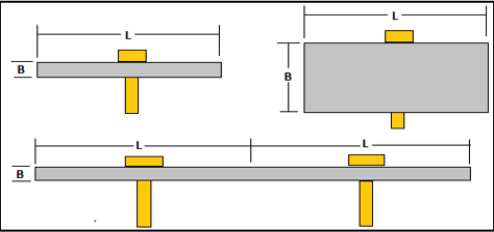
0.00E+00 Parabolic shear  $3*Test\ Load/2*area \leq Shear$ :

Nut And Bolt	EQ
Centerline Inserts	EQ
mm	N/A
	N/A
Single Layer	N/A
H-Shape	N/A
L-Shape	N/A
U-Shape	N/A
Rectangular Tube	N/A
	N/A

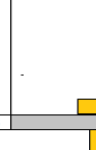
Select the tab shape and enter (b), (l), (t), and (h) according to the shape.

ns: EV Acc tab AY28-BI28	Mount thickness (B):	mm
	Mount length (L):	mm
	Minimum gusset thickness (T):	mm
	Minimum gusset height normal to mount face (H):	mm

これらの絵は、「グレーのハッチング面が溶接面」と解釈する。



CROSS SECTION	SINGLE LAYER
MOUNT THICKNESS (B)	B
MOUNT LENGTH (L)	L
MINIMUM GUSSET THICKNESS (T)	L
MINIMUM GUSSET HEIGHT (H)	B

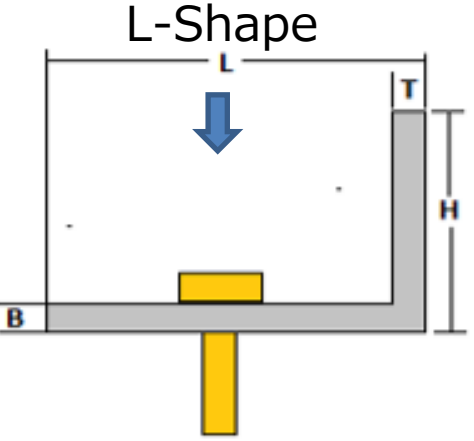
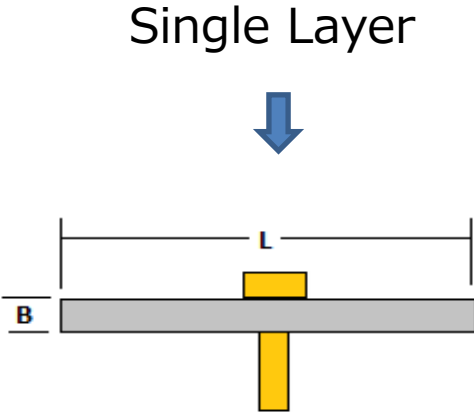
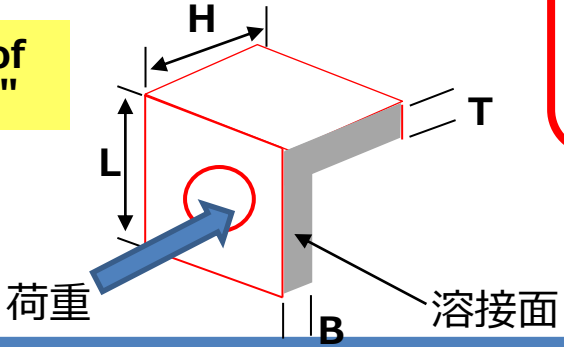


	L-SHAPE
(B)	B
(L)	L
(T)	T
(H)	H

H-SHAPE	
(B)	B
(L)	L
(T)	$\min (T1, T2, T3, T4)$
(H)	$\min (H1, H2)$

Example of "L-SHAPE"

U-SHAPE	
(B)	B
(L)	L
(T)	$\min (T1, T2)$
(H)	$\min (H1, H2)$



Interpreted as a load in the direction of the arrow on the welded surface of the gray, and consider how to attach the TAB to the FBH.



Attach the requested evidence

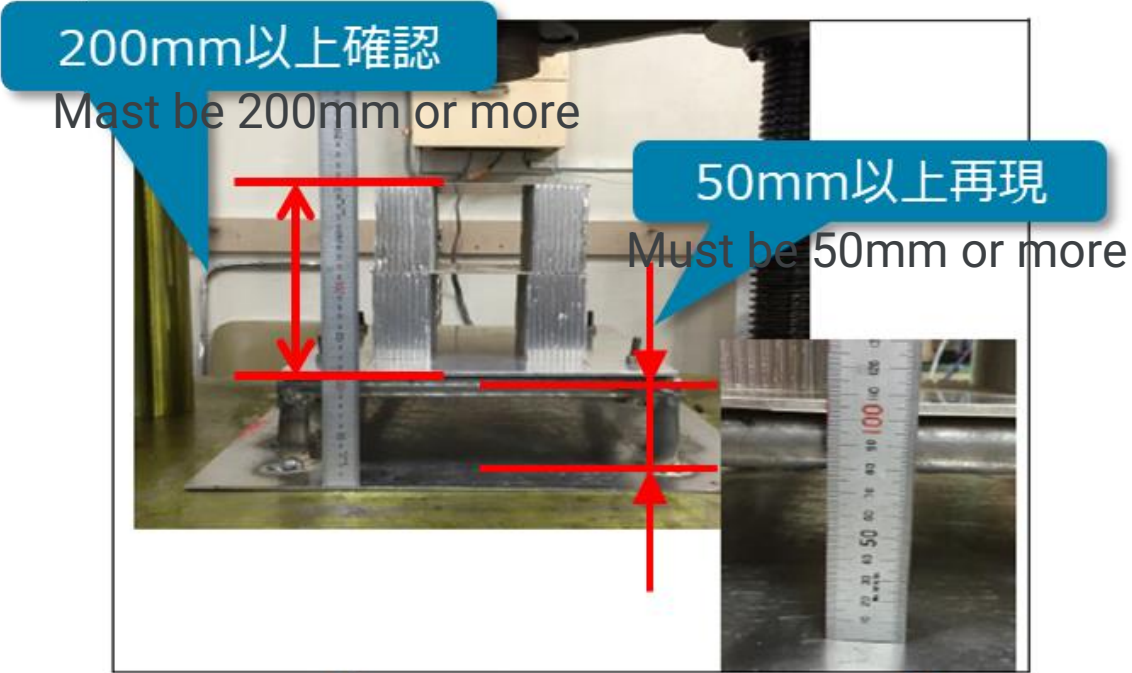
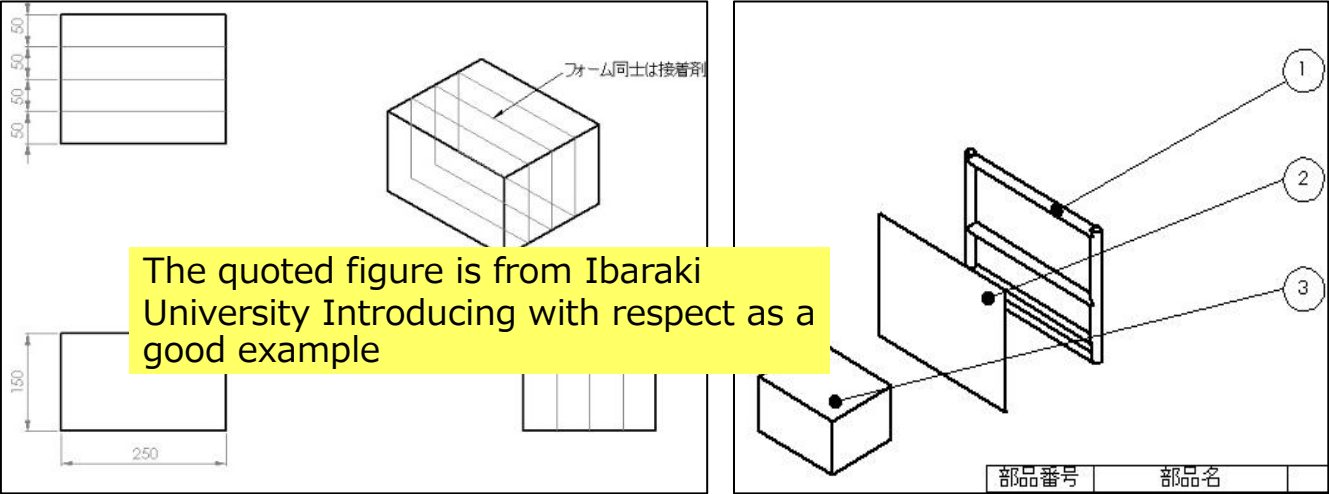
Describe diagrams and photos that shows the required dimensions

BLANK

## Physical Test Fixture Guidance

**F.8.7.6.b** The tested IA must be attached to a structurally representative section of the chassis.

BLANK				
<b>F.8.7.6.c</b> <b>F.8.4.2.a</b> <b>F.8.4.2b</b>	Front Bulkhead Outside to Outside Height:	0	mm	BLANK
	Front Bulkhead Outside To Outside Width:	0	mm	BLANK
	Fixture Thickness on table $\geq 50$ mm:		mm	BLANK
	Tested IA starting length $> 200$ mm:		mm	BLANK
	Custom IA WIDTH over 200mm length $\geq 200$ mm:		mm	N/A
	Custom IA HEIGHT over 200mm length $\geq 100$ mm:		mm	N/A



The input items are different between quasi -static and Dynamic The input is completed in all the blanks required for each, and the judgment must be "EQ"

## Impact Attenuator And / Or Wing Failure Test

BLANK			
Type of test used?:			BLANK
Name of Test Facility:	Quasi Static		BLANK
Dates of test:	Dynamic		BLANK
Maximum crushed displacement:	0	mm	REJECT
Post crush displacement, demonstrating any springback:		mm	BLANK
Crushed attenuator height:		mm	BLANK
AI plate deformation:		mm	BLANK

F.8.8.6.d

F.8.8.2.b All calculated values must be based on a mass of 300kg and an initial velocity of 7m/s.

F.8.8.8.a Average deceleration from a dynamic test must be calculated from raw, unfiltered data

F.8.8.8.b Peaks above 40g must not be seen after the application of specific filtering. See rule.

F.8.8.2b The impact attenuator must absorb at least 7350J. Springback may be ignored.

Make sure to use stepwise integration:  $\text{current\_force} * (\text{current\_disp} - \text{prev\_disp}) + \text{previous\_total}$

Do not assume steps are identical. Use similar procedure for average force.

INCORRECT:  $\text{Final\_force} * \text{final\_displacement}$ , or negative energy slope when there is positive force

BLANK				
F.8.8.2a	Peak attenuator force:	0	N	EQ
	Peak attenuator only deceleration $\leq 40g$ :	0	g	BLANK
	Average attenuator force:	0	N	EQ
	Average attenuator only deceleration $\leq 20g$ :	0	g	EQ
F.8.8.2b	Energy absorbed $\geq 7350J$ :	0	J	REJECT
	Energy absorption check:	7350	J	EQ

EQ	EQ	EQ
	EQ	
	EQ	

## Composite AIP 120kN Physical Test

Teams may use a crushed attenuator of the version installed on the car to test a composite AIP. Split the data following the IA test for the IA sections above and the 120kN test below.

EQ			
Type of test used?:			N/A
Name of Test Facility:			N/A
Dates of tests:			N/A
Maximum crushed displacement:		mm	N/A
Post crush displacement, demonstrating any springback:		mm	N/A
AI plate deformation:		mm	N/A
F.8.3.1.b	Maximum AIP force $> 120kN$ :	N	N/A

## Attach the requested evidence

Insert Test Pictures - may be added below:

- (a.) IA and FB test fixture before the test (F.8.7.4.d) which also shows the method of spacing AIP at least 50mm from any rigid structure (F.8.7.6.c)
- (b.) IA, Anti-Intrusion Plate after the IA test (F.8.7.4.d) which shows the deflection was less than 25.4mm (F.8.7.6.d)
- (c.) IA / AIP Force Displacement Curve
- (d.) IA Energy Displacement Curve

BLANK

F.8.4.3.b

F.8.7.7.b

Imp

Attach a photo that can prove the "Dates of Tests" test date. (Take a picture of what you can see in the photo together)

star\_border

BLANK

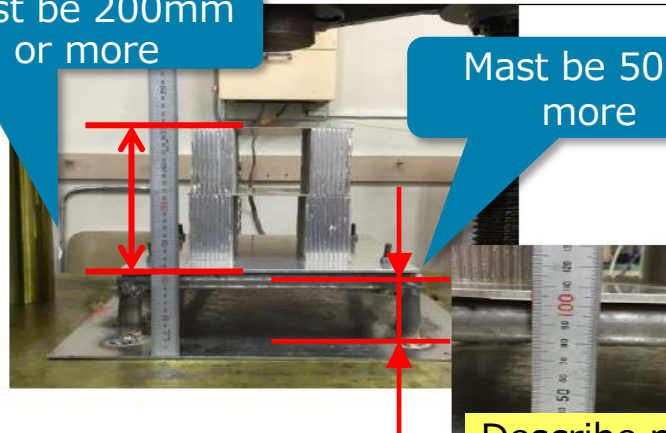
BLANK

BLANK

tests:

Mast be 200mm or more

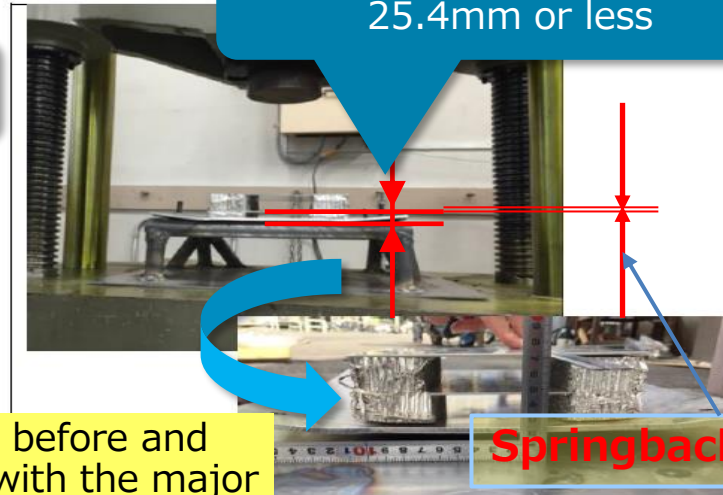
Mast be 50 or more



Describe photos before and after the exam with the major

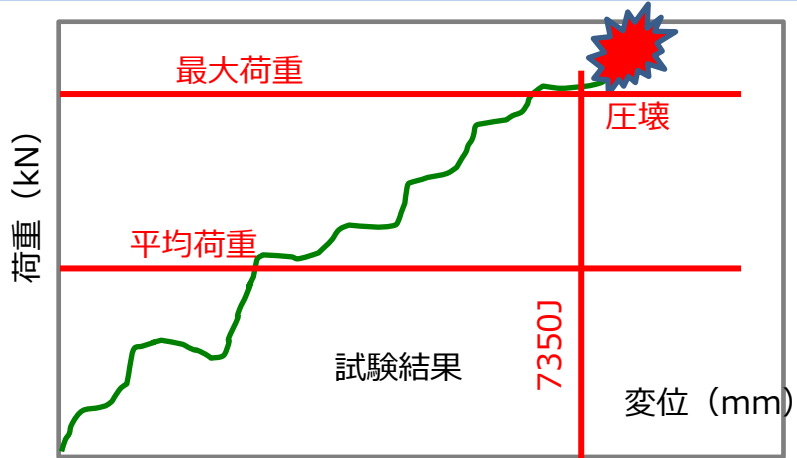
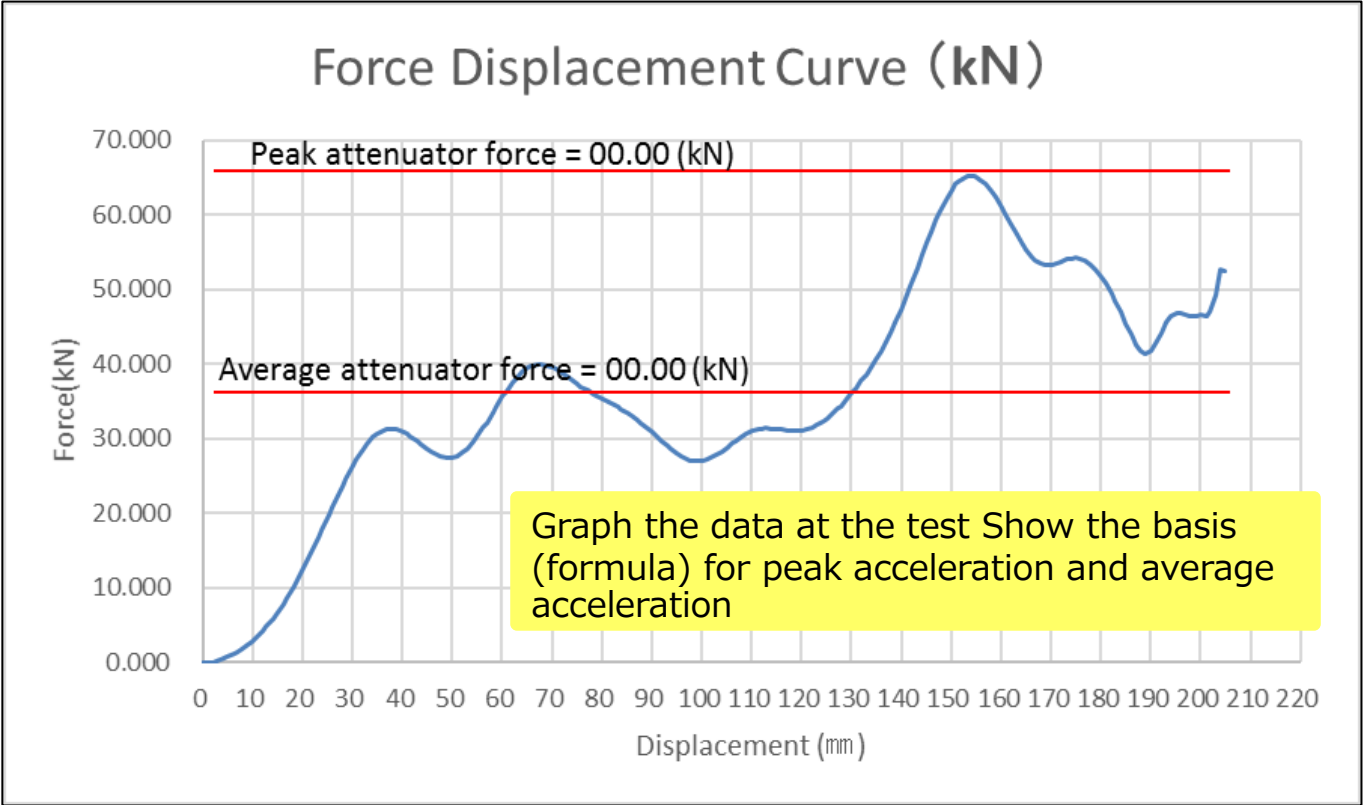
- ① Photo before the impact Attenuator test
- ② Reproduce 50mm or more from the penetration prevention board, and put an impact Attenuator on it.

The deformation amount is 25.4mm or less



Springback amount

- ① Photo after the impact Attenuator test
- ② Measure the amount of deformation of the AIP
- ③ Measure the springback amount of IA



Paste in logged data from test below:  
It is acceptable to resample the data at a lower frequency to reduce the number of datapoints. Repeat the weighted average force and energy calculations in columns three and four. Do not assume all steps are three and four. Do not assume all steps are

Disp. mm	Force N	Weighted Average Force	Energy J
MAX	MAX	MAX	MAX
15	6511	N	12.386
0	0	0	0
1	4	4	0.004

It is recommended to fill in the data every 1 mm It is recommended to show the formula of how the average load and absorption energy were asked.

9	2421		4.153
10	2813		5.234
11	3694		6.507
12	4186		7.88
13	4713		8.899
14	5875		10.588

Indicates data up to the maximum amount

Continuously compress the attenuator with a compressed test machine, and the reaction force (kN) for the stroke (mm) at that time is determined. The ultimate energy requires that the energy required for a small deformation (measured force \* deformed unit length deformation) is piled up and eventually becomes more than 7350J determined by the rule.

$$\text{Energy} = F [\text{N}] * S [\text{m}] = F [\text{kN}] * 1000 * S [\text{mm}] / 1000$$

$$\text{Deceleration} = F [\text{N}] / 300\text{kg} * 9.8\text{ms} = F [\text{N}] / 2940 = \bigcirc \text{G}$$

以下のサンプルを参考にIADを資料を作成する

Impact Attenuator Energy calculation sample sheet			
measuring data1			
		Energy=F*Displacement [J]	
		unit [N*m]	
Displacement [mm]	Force [kN]	Energy [J = kN*1000*mm/1000]	
0	0	0	
1	10	10	
2	20	30	
3	30	60	
4	31	91	
5	29.4	120.4	
6	33	153.4	
7	35	188.4	
8	36	224.4	
9	38	262.4	

Attach the test data

measuring data2

